



Thermal Characterization of Convective Heat Transfer in Microwires Based on Modified Steady State “Hot Wire” Method

Xiaoman Wang^{1,2#}, Rulei Guo^{1,2#}, Qinqing Jian^{1,2#}, Guilong Peng^{1,2}, Yanan Yue³ and Nuo Yang^{1,2*}

The convection plays a very important role in heat transfer when MEMS work under air environment. However, traditional measurements of convection heat transfer coefficient require the knowledge of thermal conductivity, which makes measurements complex. In this work, a modified steady state “hot wire” (MSSHW) method is proposed, which can measure the heat transfer coefficient of microwires' convection without the knowledge of thermal conductivity. To verify MSSHW method, the convection heat transfer coefficient of platinum microwires was measured in the atmosphere, whose value is in good agreement with values by both traditional measurement methods and empirical equations. Then, the convection heat transfer coefficient of microwires with different materials and diameters were measured by MSSHW. It is found that the convection heat transfer coefficient of microwire is not sensitive on materials, while it increases from 86 W/(m²·K) to 427 W/(m²·K) with the diameter of microwires decreasing from 120 μm to 20 μm. Without knowing thermal conductivity of microwires, the MSSHW method provides a more convenient way to measure the convective effect.

Keywords: Hot wire method; Micro wire; Convection heat transfer coefficient; Size effect; Thermal conductivity

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Introduction

With the prosperous development of micro-electro-mechanical systems (MEMS), heat dissipation within highly integrated circuits has drawn wide attention.¹ The chip-level heat generated by the increasing power density is pushing the demand of better cooling methods.² If the trend of integration and miniaturization keeps following the International Technology Roadmap for Semiconductors (ITRS), thermal management will become the bottleneck for further development of the electronic devices.^{2,4} In the past two decades, the heat transfer in one-dimensional (1-D) structures has been investigated, which are widely employed in MEMS. It is important for understanding the thermal properties of materials,^{5,6} enhancing heat transfer in MEMS theoretically and experimentally,^{7,9} and enriching applications in energy conversion, such as nanowire solar cell^{10,11} and thermoelectric application.^{12,13}

According to previous works, there are several methods to measure the thermal conduction of 1-D microwires including the steady-state hot wire method,¹⁴ the 3ω method¹⁵⁻¹⁷ and the Raman spectroscopy method.¹⁸⁻²⁰ Among these methods, the steady-state hot wire method is one of the most convenient and simplest method to

measure the thermal conduction of 1-D structure. To exclude convective heat transfer effect, these approaches are normally carried out in a vacuum environment.

Besides the thermal conduction, convective heat transfer has also been investigated. It has been proved that the convection shows different performances when the size of sample shrinks to micro/nanoscale. For example, convection heat transfer coefficient continuously increases from 5 ~ 10 W/(m²·K) (natural convection on bulk material)²¹ to over 4000 W/(m²·K) (micro carbon fiber with a diameter of 4.3 μm).²² Moreover, convection heat transfer coefficient of carbon nanotubes with a diameter of 1.47 nm can reach 8.9×10^4 W/(m²·K) in an atmosphere environment.²³ Such high convection heat transfer coefficient under micro/nanoscale indicates that the convection plays a significant role in heat dissipation in MEMS devices.

There are three main methods to measure the convection heat transfer coefficient of 1-D structure. The first one is the modified 3ω method.²⁴ By adding convection part into the original model, the convection heat transfer coefficient can be measured when other thermal properties are known, including thermal conductivity. The second one is Raman mapping measurement. By comparing Raman temperature measurement result with the value from resistance change by joule heating, Zhang's group searched for the optical absorption coefficient and then use the best fitting result to get the convection heat transfer coefficient during iteration.²² The third one is taking advantage of the steady-state method to analyze the air side.^{25,26} However, this method ignores the heat conduction within the sample. Theoretical calculation has shown that the heat conduction can be overlooked only when the length of the tested sample has reached a certain value.²³

Since conductive and convective effects are coupled in heat transfer of MEMS and traditional methods ignore thermal conduction or get it by other ways, a method for characterizing convective heat

¹State Key Laboratory of Coal Combustion, Huazhong University of Science and Technology (HUST), Wuhan 430074, China

²Nano Interface Center for Energy (NICE), School of Energy and Power Engineering, Huazhong University of Science and Technology (HUST), Wuhan 430074, China

³School of Power and Mechanical Engineering, Wuhan University, Wuhan 430072, China

#XW, RG, and QJ contribute equally on this work.

*E-mail: nuo@hust.edu.cn

transfer effect without the knowledge of thermal conduction is convenient and important. Yue *et al.* proposed a method to study conductive and convective heat transfer of microwires simultaneously by using steady-state Joule-heating and Raman mapping together.⁷ However, the expensive Raman equipment and the relatively large signal error limit its broader application.

In this paper, we proposed a modified steady state hot wire (MSSHW) method which can characterize convection heat transfer coefficient of microwires without the knowledge of thermal conductivity. Firstly, we theoretically derived the mathematical model of MSSHW method. Secondly, we measured convection heat transfer coefficient of a platinum microwire to verify MSSHW method. Then, using MSSHW method, we studied the material dependence of convection heat transfer coefficient by measuring microwires of platinum, stainless steel and tungsten. Lastly, microwires with different diameters ranging from 20 to 120 μm were measured to study the size effect on convection heat transfer coefficient. This work presents a convenient experimental method, MSSHW method, to study the heat transfer at microscale by convection.

Model & Method

The schematic illustration of experimental setup is shown in Fig. 1a.

The sample is connected to a multimeter (Keithley 2700) and a current Source (Keithley 6221) in a four-electrodes configuration. A direct current is applied on the two outside electrodes and the corresponding voltage is measured on the two inside electrodes, which diminishes the contact electric resistance. The photo of experimental setup is shown in Fig. 1b.

When a direct current is applied to an electroconductive microwire, the microwire will heat itself up due to Joule heating. The temperature increase is closely related to both the conduction and the convection of the microwire, when the radiation can be neglected. When a series of microwires with different length has been measured, the thermal conductivity can be eliminated from the calculation of convection heat transfer coefficient. Thus, it provides a possibility to measure the convection heat transfer coefficient without knowing thermal conductivity.

The heat transfer in a microwire can be described by 1-D heat transfer equation as:

$$\kappa A \frac{d^2 T(x)}{dx^2} - hP(T(x) - T_E) - \varepsilon \sigma P(T^4(x) - T_E^4) + qA = 0 \quad (1)$$

where κ is the thermal conductivity, A is the cross area, h is the convection heat transfer coefficient, T_E is the environment temperature,

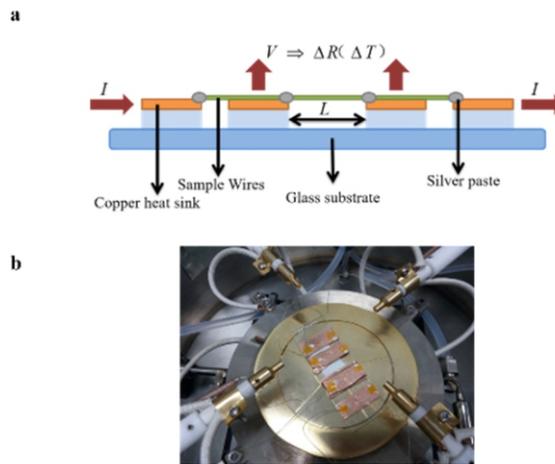


Fig. 1 (a) The sketch schematic illustration of experimental setup with a four-electrodes configuration (not to scale). (b) Photo of experimental setup.

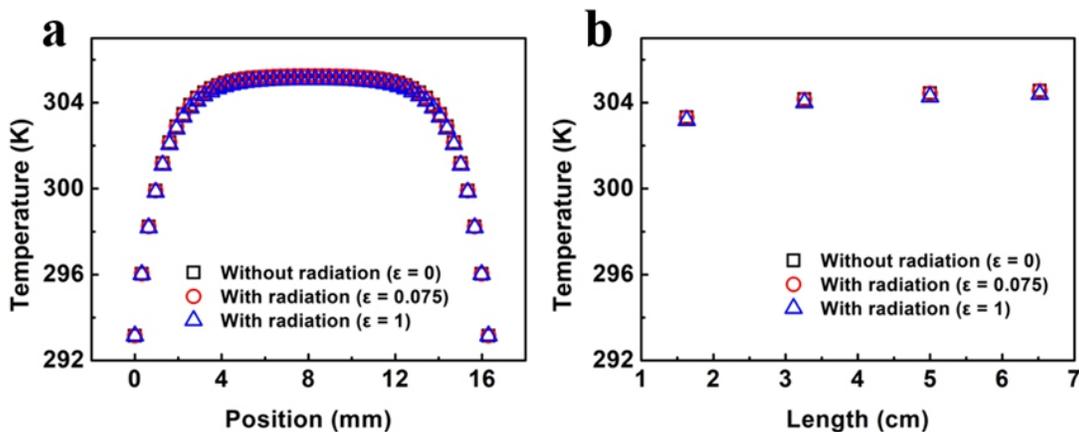


Fig. 2 (a) The temperature distribution for platinum wire with $d = 32.6 \mu\text{m}$, $l = 16.3 \text{ mm}$ under the current of 60 mA with and without radiation effect considered. (b). Average temperatures for platinum wires with different lengths ($d = 32.6 \mu\text{m}$). Black squares represent values when radiation effect is ignored. Red circles represent values when radiation effect with an emissivity of 0.075 is considered. Blue up triangles represent values when radiation effect with a maximized emissivity of 1 is considered.

P is the perimeter, ε is the emissivity, σ is the Stefan-Boltzmann constant as $5.67 \times 10^{-8} \text{ W}/(\text{m}^2 \cdot \text{K}^4)$, and q is the heat generated per unit volume. The four terms in the left side represent the thermal conduction, the natural convection, the radiation and the heat generated inside the thin wire, respectively. The thermal conductivity of wire is much higher than that of air, and the ratio of length to diameter is large (about 100), so it is acceptable to neglect the radial temperature gradience.

The contribution from radiation is much smaller than that from conduction and convection, which can be therefore neglected. To confirm this assumption, the temperature profiles were calculated with/without radiation according to Eq. 1 by MATLAB. The calculated sample is a platinum microwire, whose length and diameter are 16.3 mm and 32.6 μm , respectively.²⁴ The size of the calculated sample is a typical situation in the real experiments. By applying $\kappa = 66.5 \text{ W}/(\text{m} \cdot \text{K})$, $h = 410 \text{ W}/(\text{m}^2 \cdot \text{K})$ ²⁴ and $\varepsilon = 0.075$ into Eq. 1,²⁷ we can get the temperature profile of the wire as shown in Fig. 2a (shown as red circles). We calculated the average temperature of four microwires with different lengths as shown in Fig. 2b, and radiation shows negligible influence on the temperature profile of those microwires. The surfaces of the wires used in our experiment are all polished, so the emissivity is small ($\varepsilon < 0.1$). To show the thermal radiation is fairly neglectable, the temperature distribution for platinum wire (Fig. 2a) is plotted. As the Fig. 2a shown, even if the emissivity is maximized to be 1, the difference of temperature distribution is still very small ($< 1.5\%$). It is difficult to point out that the relationship between the thermal radiation and diameters/ lengths, because the radiation is also closely related to the temperature rise of the wire. As the diameter increases, the convection heat transfer coefficient will decrease. Therefore, the ratio of heat transferred by radiation to heat transferred by convection will increase. So, larger the diameter is, more important role the radiation plays.

Thus, the 1-D heat transfer equation can be simplified as

$$\kappa A \frac{d^2 T(x)}{dx^2} - hP(T(x) - T_E) + qA = 0 \quad (2)$$

Thus, the 1-D heat transfer equation can be simplified as

$$\begin{cases} T(0) = T_E \\ T(L) = T_E \end{cases} \quad (3)$$

where L is the length of the microwire.

The solution of the 1-D heat transfer equation is

$$T(x) = T_E + \frac{q}{\kappa A} + \frac{\left(-\frac{q}{\kappa A} e^{2mL} + \frac{q}{\kappa A} e^{mL}\right) e^{-mx} + \left(-\frac{q}{\kappa A} e^{mL} + \frac{q}{\kappa A}\right) e^{mx}}{e^{2mL} - 1} \quad (4)$$

$$m = \sqrt{\frac{hP}{\kappa A}}$$

Then, $T(x)$ is integrated over the length and the average temperature increase is calculated as

$$\Delta T = \frac{1}{L} \int_0^L T(x) dx - T_E = \frac{q}{\kappa m^2} \left(1 - \frac{2(e^{mL} - 1)}{mL(e^{mL} + 1)}\right) \quad (5)$$

It is noticed that, when the characteristic length of sample is in microscale, $e^{mL} \gg 1$. Then, the right side of Eq. 5 can be simplified as

$$\Delta T = \frac{q}{\kappa m^2} \left(1 - \frac{2}{mL}\right) \quad (6)$$

The error made from this simplification is within 0.001%.

Moreover, the resistance change caused by the average temperature change can be described with resistance change rate with temperature $\frac{dR}{dT}$ ²⁸

$$\Delta R = \frac{dR}{dT} \Delta T = \frac{dR}{dT} \frac{q}{\kappa m^2} \left(1 - \frac{2}{mL}\right) \quad (7)$$

The resistance change rate with temperature $\frac{dR}{dT}$ can be calculated using temperature coefficient of resistance β shown as Eq. 8.²⁸

$$\frac{dR}{dT} = \beta R_0 \quad (8)$$

where R_0 is the resistance of the microwire at the environment temperature, and it can be calculated as²⁸

$$R_0 = \rho \frac{L}{A} \quad (9)$$

where ρ is the electrical resistivity.

The heat generated per unit volume q is calculated using Joule's first law

$$q = \frac{I^2 R}{V} = \frac{I^2 R}{AL} \approx \frac{I^2 R_0}{AL} = \frac{I^2 \rho \frac{L}{A}}{AL} \quad (10)$$

where V is the volume of the wire sample.

Then Eq. 7 can be expressed as:

$$\begin{cases} \Delta R = \alpha L - b \\ \alpha = \frac{\beta I^2 \rho^2}{A^3 \kappa m^2} \\ b = \frac{2\beta I^2 \rho^2}{A^3 \kappa m^3} \end{cases} \quad (11)$$

It shows that there is a linear relationship between the increase of resistance and the length of samples.

Based on Eq. 11, the main equations of MSSHW method are derived out as

$$h = \frac{16\beta I^2 \rho^2}{\pi^3 d^5 \alpha} \quad (12)$$

where d is the diameter of the thin wire and I is the given current. That is, convection heat transfer coefficient (h) can be obtained by measuring linear relationship between ΔR and L without knowing thermal conductivity.

Based on Eq. 11, the thermal conductivity can also be calculated as

$$\kappa = \frac{16\beta I^2 \rho^2 \cdot b^2}{\pi^3 d^6 \alpha^3} \quad (13)$$

However, the equation of κ includes the intercept b which is a very small value compared with ΔR . The value of b is so small that it is highly uncertain. So that the thermal conductivity κ calculated by this equation has a high uncertainty. Therefore, we don't discuss the thermal conductivity here.

The thermal and electric resistances between the two inner probes and substrate will make the measured temperature higher than that in the ideal condition. The longer the wires are and the more heat the wires generate, the higher the temperature increment at the contact

position will be. This leads to a larger slope of the linear relationship between the increase of resistance and the length of samples. As a result, the measured convection heat transfer coefficient will be underestimated. To address this problem, two techniques were utilized. The first one is that the four-point-probe technique is chosen, instead of two-point-probe, in the experiment. With the four-point-probe technique, the applied current cannot go through the contact point between the two inner probes and substrate. Thus, there is no joule heat generated at those contact points. The second one is that silver paste is applied at those contact points. With silver paste, as stated in other works,^{29,30} the electrical/thermal contact resistance can be minimized.

To proof the validity of MSSHW method, the natural convection heat transfer coefficient of platinum microwires were measured. Firstly, the diameters of the platinum wire were measured by optical microscope and the picture is shown in Fig. 3b. By averaging around 200 measured values at different positions of the microwire, the diameter of the platinum wire is obtained as $41 \pm 3 \mu\text{m}$. Secondly, by measuring their resistances, the lengths of the samples are obtained based on Eq. 9.²⁸ Thirdly, the increase of electric resistance (ΔR) of seven samples, whose lengths range from 20 mm to 130 mm, were

measured under the current of 60 mA (shown as red open circles in Fig. 4a). Finally, in accordance with Eq. 11, the parameters of a and b can be obtained by linear fitting. When the current was applied as 60 mA, a and b were obtained as $2.41 \pm 0.02 \Omega/\text{m}$ and $0.015 \pm 0.002 \Omega$, respectively. Therefore, convection coefficient can be calculated out by Eq. 12 as $246 \pm 60 \text{ W}/(\text{m}^2\cdot\text{K})$. The large uncertainty of the convection coefficient (around 30%) is due to the large uncertainty of diameter measurement. The uncertainty of diameter measurement mainly comes from the non-uniformity of the wire and the limited resolution of an optical microscope. So, to reduce the uncertainty, more uniform wires should be used and more precise methods, such as scanning electron microscope (SEM), should be used to measure the diameter. If a precise diameter is available, the uncertainty will be around 3%. In addition, to show the linear relationship between the increase of electric resistance and the wire length is general, the values of samples with different materials and different diameters are also plotted in Fig. 4a.

The convection heat transfer coefficient, measured under different direct current, are shown in Fig. 4b. As the results show, the convection coefficient is current independent. Of course, the current can't be too high or too low. In this work, the temperature rise is controlled between

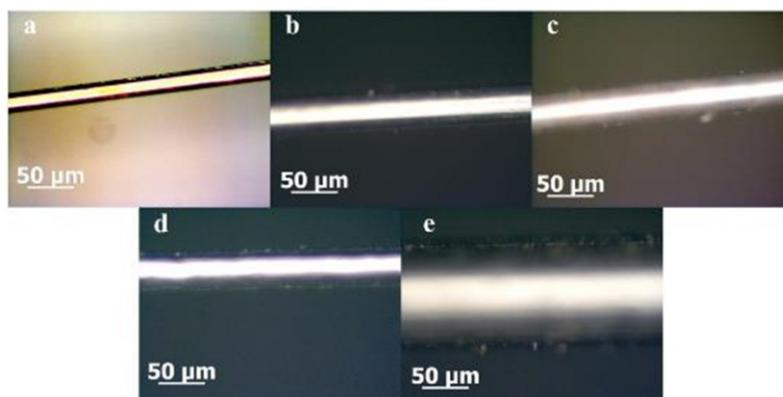


Fig. 3 The microscope photo of microwires (the diameter is measured from at around 200 different positions of those microwires): (a) platinum: $20 \pm 1 \mu\text{m}$ in diameter; (b) platinum: $41 \pm 3 \mu\text{m}$ in diameter; (c) Tungsten: $40 \pm 1 \mu\text{m}$ in diameter; (d) stainless steel: $42 \pm 2 \mu\text{m}$ in diameter. (e) stainless steel: $120 \pm 6 \mu\text{m}$ in diameter.

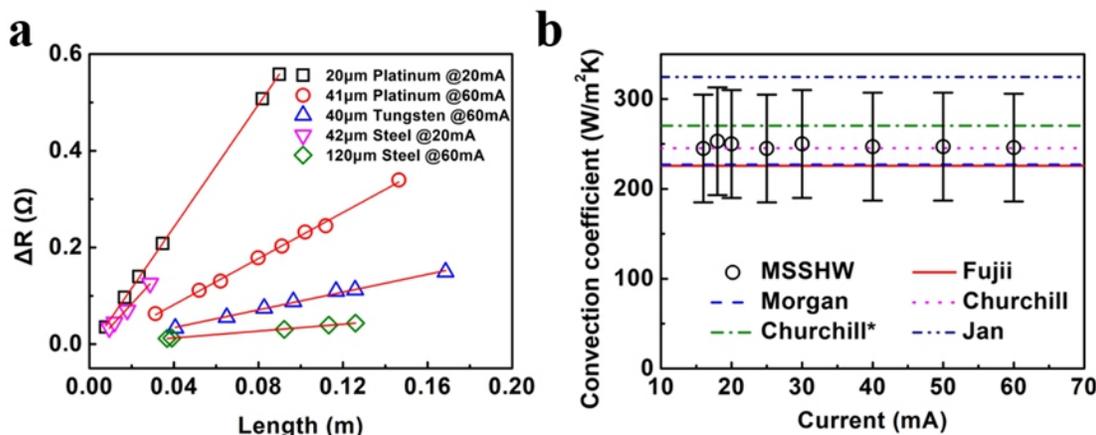


Fig. 4 (a) The increase of electric resistance with length. The black squares are ΔR of platinum wires with a diameter of $20 \mu\text{m}$ and applied 20 mA current; the red circles are ΔR of platinum wires with a diameter of $41 \mu\text{m}$ and applied 60 mA current; the blue up triangles are ΔR of tungsten wires with a diameter of $40 \mu\text{m}$ and applied 60 mA current; the magenta down triangles are ΔR of steel wires with a diameter of $42 \mu\text{m}$ and applied 20 mA current; the green diamond are ΔR of steel wires with a diameter of $120 \mu\text{m}$ and applied 60 mA current. (b) Experimental results of convection heat transfer coefficient with variable current. The black open circles represent values of convection coefficient results from our work (MSSHW method). The red solid line, blue dash line, magenta dot line, green dash-dot line and navy dash-dot-dot line are convection heat transfer coefficient calculated from the empirical equations of Fujii³² Morgan,³³ Churchill,³⁴ Churchill*³⁴ and Jan,³⁵ respectively.

1 K and 5 K by choosing an appropriate electric current. On one hand, to minimize the influence of radiation, the temperature rise of the wire cannot be too high. On the other hand, the temperature rise cannot be too much smaller because the uncertainty of temperature rise measurement will be large, and even the linear relationship between the increase of electric resistance and the wire length will be not observable. Our results of convection coefficient agree well with values calculated by the empirical equations of Churchill, Morgan and Fujii. However, our results have a slight difference between Jan's empirical equation.³¹ The difference can be attributed to the following factors: thermal conduction to the supports and the temperature measurement locations; distortion of the temperature and velocity fields by bulk fluid movements; the use of undersized containing chambers or the presence of the temperature system and supports; and temperature loading effects.³²

To study the material effect on the convection heat transfer coefficient, microwires ($\sim 40 \mu\text{m}$ in diameter) of platinum, tungsten, and stainless steel (Fig. 3 b, c, d) are measured with MSSHW method. As shown in Fig. 5a, the values of convection heat transfer coefficient are independent on materials. The values of three materials with $40 \mu\text{m}$ diameter are close to each other, which is also close to the prediction

values in Ref.^{32,34} by empirical equations. According to the optical microscope images, the slight difference in convection coefficients may be attributed to the surface roughness which has influence on heat convection.³⁶

Moreover, microwires with different diameters were measured to show the size effect of convection heat transfer coefficient (Fig. 5b). As we can see, the diameter largely affects convection heat transfer coefficient. With diameter decreasing from $120 \mu\text{m}$ to $20 \mu\text{m}$, the convection heat transfer coefficient increases from $86 \text{ W}/(\text{m}^2\cdot\text{K})$ to $427 \text{ W}/(\text{m}^2\cdot\text{K})$. The measured convection heat transfer coefficients increase sharply when the diameter decreases. This phenomenon might attribute to the inadequate development of the boundary layer. For a horizontal wire with a diameter larger than $10 \mu\text{m}$, the heat is carried away by continuous gas fluid and the noncontinuous layer can be ignored, and the continuum assumption is valid.³⁷ Then, it is shown that the concept of boundary layers is central in understanding of convection heat between a surface and a fluid flowing past it.³⁵ The boundary layer is defined as the region of the fluid in which the temperature gradient exists. Because a thicker boundary layer, which means a smaller wall temperature gradient, leads a smaller rate of heat transfer across the boundary layer, h decreases with increasing boundary layer. For a

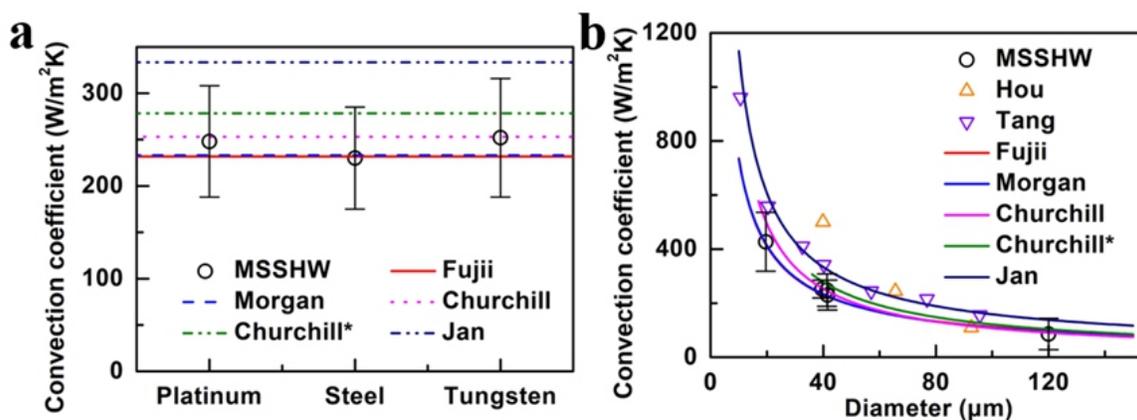


Fig. 5 (a) The natural convection heat transfer coefficients of the three microwires with different materials measured by MSSHW method. The diameter of platinum, stainless steel and tungsten microwires is $41 \mu\text{m}$, $42 \mu\text{m}$ and $40 \mu\text{m}$, respectively. (b) Experimental convection heat transfer coefficients under different diameters measured by MSSHW method. (black open circles were measured results by MSSHW method, the orange up triangles were measured by Hou,²⁵ and the purple down triangles were measured by Tang.²⁴)

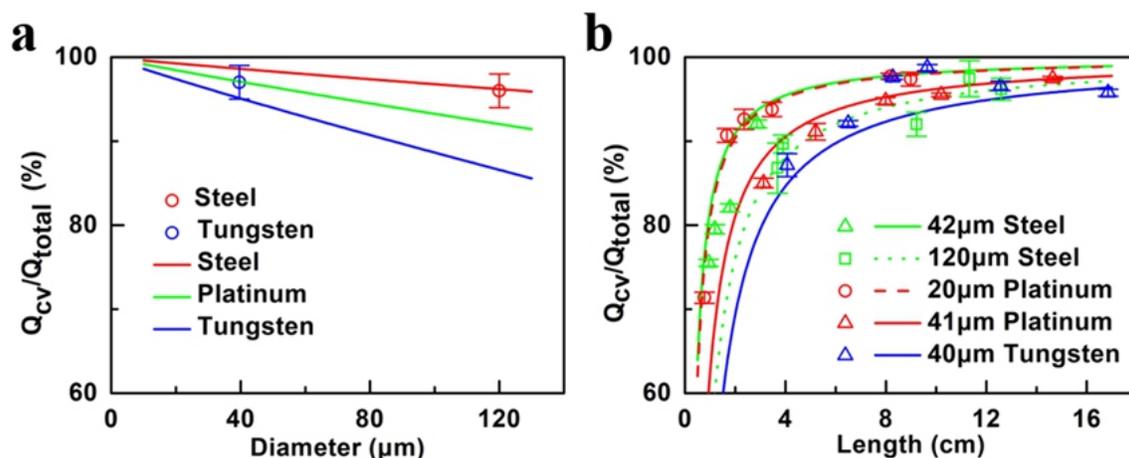


Fig. 6 (a) The percentage of convection heat transfer under different diameters. The length of those microwires is $\sim 126 \text{ mm}$ (dots are measured results by MSSHW method and calculated by Eq. 14; lines are calculated by Eq.15 with parameters from Ref.33). (b) The percentage of convection heat transfer under different lengths.

horizontal cylinder wire, the boundary layer starts from the bottom of the wire and ends on the top with a plume ascending from the wire (shown in Fig. 9.8 in Ref 35). So, the boundary layer is thinnest at the bottom of the wire and then becomes thicker due to the heating of the wire. As a result, for a wire with smaller diameter, the boundary layer will be more inadequate, which means that the average boundary layer will be thinner and the h will be larger. In comparison, both experimental results^{24,25} and empirical equations results^{32,35} are also shown in Fig. 5b.

To get a better understanding of heat transfer in microscale, the percentage of heat transferred by convection (Q_{cv}/Q_{total}) has been investigated. Based on Eq.2 and Eq.10, Q_{cv}/Q_{total} can be obtained by measurements as

$$Q_{cv}/Q_{total} = \frac{hPL\Delta T}{I^2R} \quad (14)$$

Besides, from Eq. 5, the value of ratio can also be estimated as

$$Q_{cv}/Q_{total} = \frac{hPL\Delta T}{qAL} = 1 - \frac{2}{mL} \left(\frac{e^{mL} - 1}{e^{mL} + 1} \right) \quad (15)$$

Firstly, we studied the dependence of Q_{cv}/Q_{total} on the diameter of microwires. The data from measurements (Eq. 14) are matched well with the prediction curves by theory (Eq. 15). As shown in Fig. 6a, with the diameter decreasing, Q_{cv}/Q_{total} increases. For example, for a steel microwire with a diameter of 120 μm and a length of 126 mm, the percentage of heat flux carried by convection is more than 95%. So, convection plays a predominant role in heat transfer of microwires.

Moreover, the ratio depends on the materials, as shown in Fig. 6a. The thermal convections of microwires are not sensitive on materials. However, the thermal conduction depends on materials. The thermal conductivity of steel, platinum and tungsten microwires measured by traditional steady state hot wire method are 18 ± 3 , 79 ± 3 and 224 ± 9 W/(m·K), respectively. Because the steel microwire has a lower value of thermal conductivity than platinum and tungsten. it has a higher value of Q_{cv}/Q_{total} .

Secondly, we studied the dependence of Q_{cv}/Q_{total} on the length of microwires. Fig. 6b shows that, with the increasing of length, the ratio of Q_{cv}/Q_{total} increases. It means that the longer a wire is, the more important the convective heat transfer is. Because the area of convection increases with the length.

Conclusion

In conclusion, a modified steady-state hot wire (MSSHW) method is proposed to characterize the conductive and convective heat transfer of microwires simultaneously. The method is verified by measuring the convection heat transfer coefficient of microwires. The convective heat transfer between micro metal wires and their surrounding air environment is found to be irrelevant to material composition, but is strongly connected with the diameter of the wires. When the diameter of microwires decreases from 120 μm to 20 μm , the natural convection coefficient increases from 86 W/(m²·K) to 427 W/(m²·K). The convection coefficient is in reasonable range compared with those from the references. This MSSHW method provides a convenient way for measuring convective heat transfer of microwires without knowing thermal conduction, which is beneficial to studying the comprehensive heat transfer at microscale.

Thermal convection may play an even more important role in thermal management for the wires at the nanoscale. However, only a few experiments of thermal convection of nanowire have been reported

due to the limitation of measurement methods. The MSSHW method proposed here is possible to be applied to nanowires, because that the MSSHW method is modified from the traditional steady-state hot wire method which has been widely used to study the thermal conductivity of nanowires.

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